

Sylvain Houle
 Lawrence Keyes
 John C. King
 Stoney Klengler
 Jody Koenig
 Glenn Lundborg
 Jeff Mendenall
 Edwin L. Morgan, Jr.
 Harry Norris
 William Rathyen
 A.H. Rhodes
 Daniel Sabia
 Glen R. Shenton
 Vance Smelser
 Julius Smith III
 J.M. Soden
 Fred Stewart
 Mitch Turik
 Robert S. Warren
 David Widiger
 Stephen S. Wilson
 Joseph Zingheim

Inst. of Biomed. Eng., Univ. of Toronto, Toronto, Ont., Canada
 Box 538, Elmira College, Elmira, NY 14901
 3985 Cascade Rd. SW, Atlanta, GA 30331
 3930 Via Lucero #20, Santa Barbara, CA 93110
 110 Elm Court, Decorah, Iowa 52101
 Sandviksgatan 36 B, S-95100 Lulea, Sweden
 219 Dorado, Ridgecrest, CA 93555
 314 Vine, Chillicothe, Ohio 45601
 Box 54, Stevenson, MD 21753
 14 Zabriski St., Bayonne, NJ 07002
 64 Brook St., Cambridge G, Ont. Canada N1R 4C3
 422 Ward Ave., Mamaroneck, NY 10543
 1237 Huron St., Apt. 403, London, Ont., Canada
 1711 McDonald Ave., New Albany, Ind. 47150
 2302 Colquitt #18, Houston, TX 77006
 10303 W. 70 Terrace, Shawnee, KS 66203
 4 Betsy Ross Cir., Acton, Mass 01720
 PO Box 47, Maidstone, Ont., Canada NOR 1K0
 Linear Devices, Box 5750, San Francisco, CA 94103
 470 Seyburn Dr., Baton Rouge, LA 70808
 620 Felch St., Ann Arbor, MI 48103
 44 West Reed St., San Jose, CA 95110

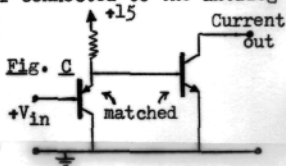
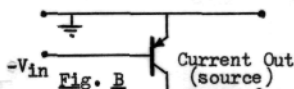
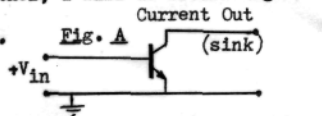
3. EXPONENTIAL CONVERTERS: -by Terry Mikulic

This paper won't deal with the actual mechanics of the antilog function. The antilog, or exponential, volt-ampere relationship of the silicon bipolar junction transistor is well documented elsewhere. Rather, I will be describing practical circuits for making use of this function.

The basic exponential converter is shown in figs. A and B. Surprised? This is all there is to it. Several things must be assumed first though. The transistors must have high D.C. gain (250 or higher), and they must be fed from a low impedance source so base currents won't cause errors. The transistors also must have low collector cutoff current (less than 10 nA).

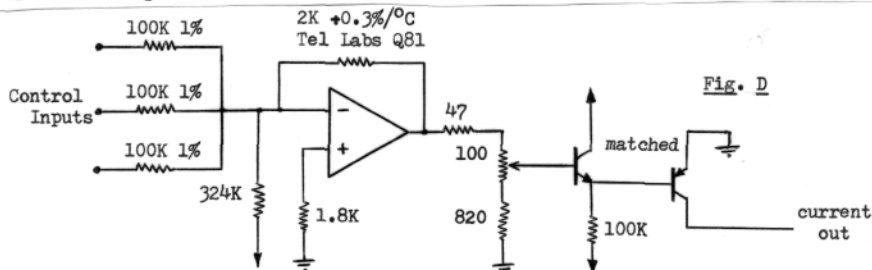
The input to output relationship of the device can be stated like this: A specific change in input voltage will produce a ratio change in output current, no matter what the value of the initial output current is. Circuit conditions for fig. A are as follows: the transistor needs a certain amount of positive input voltage, say 550 mV, which will produce an initial amount of output current, somewhere around 1 uA. Then, adding or subtracting a specific amount of voltage (at 25°C, about 18 mV) to or from the 550 mV, the output current will be doubled or halved, in that order.

Both voltage values are temperature sensitive, however. The voltage needed to produce an initial specific value of output current has a negative temperature coefficient of $-0.3\%/^{\circ}\text{C}$. The other voltage, which can be called the scale factor, has a temperature coefficient of $+0.3\%/^{\circ}\text{C}$. It has a value at room temperature of typically 18 mV. The initial positive voltage is best compensated with another transistor. A complementary polarity emitter follower connected to the antilog transistor is shown in fig. C. Assume that the input to the emitter follower is at 0V, the transistors are matched, and the gain of the transistors is high enough so that the base currents can be ignored. The collector current of any one transistor will be the same as its emitter current. Therefore, because the emitter to base voltages of the transistors are the same, the collector currents of the two



transistors are the same. Changes of emitter to base voltage due to temperature changes in one transistor are countered by the same changes in the other transistor. Applying positive or negative voltages of intervals of 18 mV will produce changes in the output current by factors of two. A linear current controlled oscillator connected to the output will produce pitch changes of octaves.

The industry standard for voltage controlled oscillators is one volt into 100k Ohms for a pitch change of an octave. Fig. D describes a circuit which adds all control voltages and reduces a 1 Volt input to 18 mV. It also provides a means of temperature compensating the scale factor, which cannot be compensated with another transistor like the initial forward base voltage. It provides a current source, which must be returned to a point more negative of the emitter of the antilog transistor. This circuit is very accurate over a wide range.



Accuracy at low collector currents is limited by the collector leakage current of the antilog transistor. A transistor selected for low leakage will extend the range. Accuracy at high collector currents is limited by the bulk emitter resistance of the antilog transistor. It can be imagined as the emitter being connected to ground through a resistor of, say 10 ohms. With currents greater than about 100 μ A, a voltage drop is produced across the resistance, which reduces the emitter to base voltage of the transistor, thereby producing less collector current than desired. The solution is to provide a positive voltage proportional to the output current and add it with the control voltages, thereby increasing the emitter to base voltage to counter the voltage drop in the emitter.

Fig. E describes a circuit which compensates for emitter resistance. The H.F. track. is adjusted for linear oscillator tracking at high frequencies.

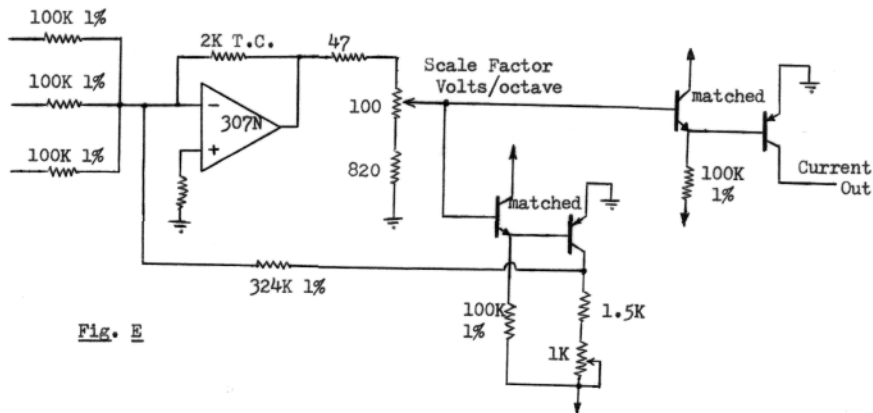
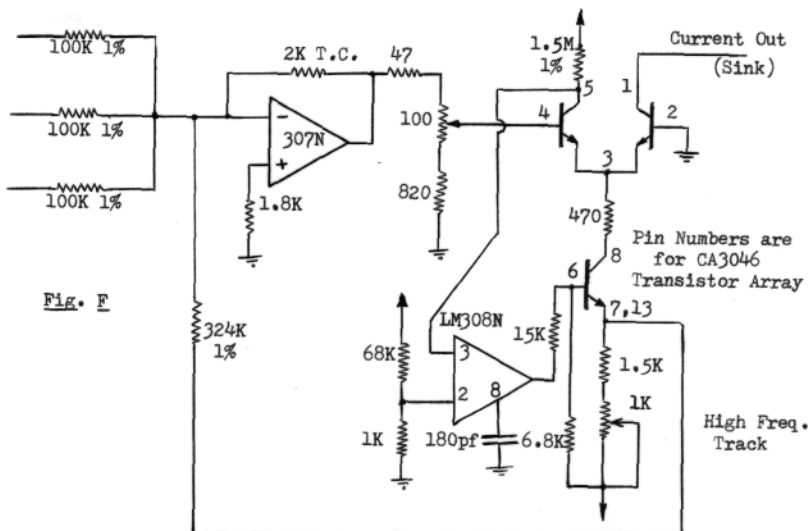
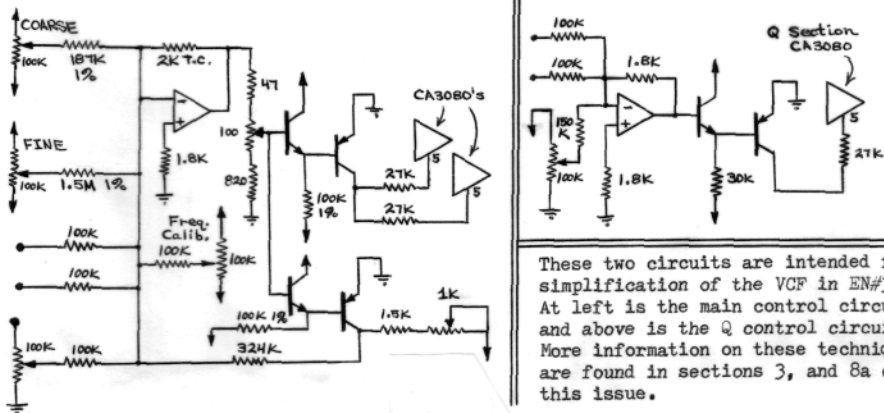


Fig. E

Fig. F



4a. READER'S EQUIPMENT: Additions to Terry Mikulic's VCF in EN#34.



These two circuits are intended for simplification of the VCF in EN#34. At left is the main control circuit, and above is the Q control circuit. More information on these techniques are found in sections 3, and 8a of this issue.